**Paper Title (16 Bold)**

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***Abstract (11 Bold)***

*The aim of this paper is to determine the effect oftemperature o linear alkylbenzene (LAB) yield from a Nigeria Refinery LAB plant. The rerun (LAB) column was simulated using Aspen HYSYS. The simulation was done at temperatures between 280oC and 360oC at temperature difference of 20oC (ΔT =20°C).*There was an *increase in the average weight percentage fraction of linear alkylbenzenes at the bottom stream temperature from 280oC to 340oC and a slight decrease at 360oC. Bottom stream temperature280oC and pressure of 115Kpa yielded the highest LAB percentage yield of 99.4%.*

***Keywords:******(11 Bold)****Rerun column Top stream temperature, Rerun column bottom streamand Linear alkylbenzene Yield.*

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1. **INTRODUCTION (10 Bold)**

Linear alkyl benzene (LAB) is a family of organic compounds with C6H6 – CnH2+1 $C\_{n}H\_{2+1}$ (n is between 10 and 16). The C12 – C15, C10 – C13 LABs are used for detergent production and are produced by the reaction between paraffins and Benzene [5]. LABs are currently being used as a liquid scintillator in neutrino detector due to its good optical transparency, its high yield, low amount of radioactive impurities and high flash points [5]. It is also a suitable material that is being used in a secret Neutrino Interaction Finder (SNIF), it is also used as an antineutrino detector design to detect the presence of nuclear reactor at a distance of 100 – 500KM [5].

After the HF acid has been stripped out by the HF stripper, the benzene in the stream is then recycled to the alkylation reactor section from the overhead of the benzene column, while n-paraffins are recycled to the PACOL unit from the overhead of the paraffin column [7, 8].

The product of alkylation unit serves as feed to the HF stripper column – after benzene has been reacted with mono-olefins to form linear alkylbenzene (LAB) in the presence of HF acid catalyst [6, 9].

Linear Alkyl benzene is a vital raw material in the production of liner alkyl benzene sulphonate [1, 2].

The LABs C10H22C6C6, C11H24C6C6, C12H26C6C6, C13H28C6C6 and C14H30C6C6 produced by the reaction between paraffins and benzene are essential raw materials for producing detergent [5, 9].

The factors that can affect biodegradability of linear alkylbezene sulphonate (Detergent) includes the structure of side hydrocarbon chain in molecule and the share of 2-phenylalkane among other isomers [4].

**1.1.1 Fractionation Section**

The light ends produced by cracking reaction are removed in the stripper column. The off -gas from the stripper is sent to the fuel gas, but flared if it is under high pressure[3]. And the paraffins and olefins in the column bottom stream are fed to the linear alkyl benzene alkylation unit. In order to recover enough heat from the bottom stream, it is necessary by passing where the paraffin stream is heated [3].

**1.1.2 Aspen HYSYS**

This is a chemical process design software or application used for designing, monitoring trouble shooting and analyzing the technical and economic performance of a chemical process plant [6].

The steps used for running flow sheet simulation in Aspen HYSYS were as follows:

1. Components selection.
2. Thermodynamic options selection.
3. Computing feeds composition and thermodynamics.
4. Creating a flow sheet.
5. Naming the feed stream.
6. Equipment parameters computation.
7. Collection of result from the simulated environment [6].



**Figure1: Linear alkylbenzene flow diagram (UOP 2009[2])**

**1.2 THE SIMULATION**

 1.2.1 The Linear alkylbenzene (rerun column) was simulated at steady state using a distillation column template of ASPEN HYSYS 8.8. Peng Robinson was selected as the fluid package.

Figure 2:represent the simulated flow diagram for the linear alkylbenzene (rerun) column



**Figure 2:Aspen HYSYS linear alkylbenzene Column Plant View**

* + 1. **Rerun column Design specifications**

Table 1 represents the rerun column design specification.

**Table 1: Rerun Column, Specification.**

|  |  |
| --- | --- |
|  | Specification |
| Striping Column diameter | 2800mm |
| Rectification Section diameter | 5600mm |
| Tray spacing | 600mm |
| Number of tray holes | 1942 |
| Hole diameter | 13mm |
| Number of Trays above feed | 15 trays, 16 stages (with condenser) |
| Number of Trays below feed | 21 trays, 22 stages (with re-boiler) |
| $Q\_{c}$ (Condenser heat duty) | 31212 MJ/hr |
| $Q\_{r}$ (Re-boiler heat duty) | 22363 MJ/h |

* + 1. **Feed Components and composition**

Table 2 indicates the LAB column feed stream components the composition in wt. % fraction.

**Table 2: Feed Components used and their Composition in weight % fraction.**

|  |  |  |
| --- | --- | --- |
| Components | Chemical Formula | Composition (wt. % fraction) |
| 1. N-Decane
 |  *n*C10H22 | 0.0003  |
| 1. N-Undecane
 |  *n*C11H24 | 0.0033  |
| 1. N-Dodecane
 |  *n*C12H26 | 0.0046  |
| 1. N-Tridecane
 |  *n*C13H28 | 0.0058  |
| 1. N-Tetradecane
 | *n*C14H30 | 0.0065  |
| 1. N-Pentadecane
 | *n*C15H32 | 0.1086  |
| 1. N-Hexadecane
 | *n*C16H34 | 0.0166  |
| 1. Decylbenzene
 | *n*C169H26 | 0.1439  |
| 1. N-undecylbenzene
 | *n*C17H28 | 0.1775  |
| 1. N-dodecylbenzene
 | *n*C18H30 | 0.2032  |
| 1. N- tridecylbenzene
 | *n*C19H32 | 0.1626 |
| 1. N-tetradecylbenzene
 | *n*-C20H34 | 0.1071  |
| 1. Heavy Alkylates
 | *n*-C26H54 | 0.0599  |

**2.2.4 Rerun column Operating Conditions**

The operating conditions of the LAB (rerun) column is as represented in table 3

**Table 3 Operating Conditions used in this Simulation are as stated below.**

|  |  |  |  |
| --- | --- | --- | --- |
|  | Feed | Top Stream (Distillate)  | Bottom  |
| Temperature °C | 178 | 93 | 232 |
|  Pressure Kpa | 200 | 9.0 | 20 |
|  Enthalpy MJ/h | -95850 | -98130 | -125900 |
|  Mass Flow-rates Kg/h | 140400 | 108900 | 14290 |

1. **RESULT AND DISCUSSION (10 Bold)**

The results obtained are as discussed below

**1.3.1 LAB Average Weight fraction.**

1. **At Top stream Operating temperatures ΔT=20oC**

The average weight fraction of n-decylbenzene, n-undecylbenzene and n-dodecylbenzene increased at the top stream operating temperature of 280oC – 300oC and decreased at 320oC – 360oC. While n-tridecylbenzene and n-tetradecylbenzene decreased at 280oC – 300oC and increased at 320oC – 360oC.

**Table 4:Average Weight fraction of LAB at Top Stream Operating Conditions ΔT=20oC.**

|  |  |
| --- | --- |
| Linear Alkylbenzenes (LAB) | Operating Temperatures( oC) |
|  | 280 | 300 | 320 | 340 | 360 |
| n-decylbenzene | 0.2792 | 0.2984 | 0.2849 | 0.2791 | 0.2740 |
| n-undecylbenzene | 0.2177 | 0.2800 | 0.2740 | 0.2714 | 0.2694 |
| n-dodecylbenzene | 0.2842 | 0.2762 | 0.2807 | 0.2820 | 0.2832 |
| n-tridecylbenzene | 0.1658 | 0.1566 | 0.1638 | 0.1675 | 0.1705 |
| n-tetradecylbenzene | 0.0885 | 0.0832 | 0.0889 | 0.0927 | 0.0950 |

**Figure 3: Average Weight fraction of LAB at Bottom Stream Operating Conditions**

1. **At Bottom stream Operating temperatures ΔT=20oC**

The average weight fraction of n-decylbenzene, n-undecylbenzene and n-dodecylbenzene increased at the bottom stream operating temperature of 280oC – 320oC and decreased at 340oC – 360oC. While that of n-tridecylbenzene and n-tetradecylbenzene remains constant. Table 4 and Fig.4

**Table 4: Average Weight fraction of LAB at Bottom Stream Operating Conditions ΔT=20oC.**

|  |  |
| --- | --- |
| Linear Alkylbenzenes | Operating Temperatures(oC) |
|  | 280 | 300 | 320 | 340 | 360 |
| n-decylbenzene | 0.2390 | 0.2393 | 0.2404 | 0.2419 | 0.2401 |
| n-undecylbenzene | 0.2558 | 0.2561 | 0.2568 | 0.2569 | 0.2568 |
| n-dodecylbenzene | 0.2797 | 0.2808 | 0.2831 | 0.2829 | 0.2837 |
| n-tridecylbenzene | 0.1897 | 0.1897 | 0.1897 | 0.1897 | 0.1897 |
| n-tetradecylbenzene | 0.1113 | 0.1113 | 0.1113 | 0.1113 | 0.1113 |

**Figure 4: Average Weight fraction of LAB at Bottom Stream Operating Conditions**

**4.2.4 LAB Average wt. % fraction Yield**

The calculated LABs percentage Yield from the average LAB weight fraction is as shown in Table 4.3

The calculated percentage yield of average LAB wt. % fraction indicated a higher percentage yield at the top and bottom stream temperature of 280oC. At this temperature the obtained yield of top and bottom streams are 92.2% and 95.3 %. Table 5 and Figure

**Table 5: LAB Average wt. % fraction Percentage Yield**

|  |  |  |
| --- | --- | --- |
| Operating \*Temperatures (0C) | Percentage Yield of Average LAB wt.% at various Top Stream operating condition | Percentage Yield of Average LAB wt.% at various Bottom Stream operating condition |
| 280 | 92.2 | 95.3 |
| 300 | 87.6 | 94.8 |
| 320 | 87.5 | 94.2 |
| 340 | 87.6 | 93.8 |
| 360 | 87.5 | 93.3 |

**Figure 5:LAB Average wt. % fraction Percentage Yield**

**5 Percentage Yield of LAB in the distillate at TBottom= 280 0C.**

* The bottom stream operating temperature of 280 0C has the highest average percentage yield of linear alkylbenzenes (LABs). The percentage yield of the linear alkylbenzene was calculated by keeping the operating temperature at 280 0C and varying the operating pressure at 17Kpa, 42Kpa, 67Kpa, 92Kpa and 115Kpa. The highest yield obtained is 99.4% which is at 115Kpa. This is as shown in Table 6. And figure 6

**Table 6: Percentage Yield of LAB in the distillate.**

|  |  |
| --- | --- |
| Pressure Kpa | Percentage Yield Of LAB in the Distillate |
| 17 | 89.1% |
| 42 | 95.4% |
| 67 | 97.9% |
| 92 | 98.97% |
| 115 | 99.4% |

**Fig.6:LAB % Yield at TBottom= 280oC.**

1. **CONCLUSION (10 Bold)**

It was observed that the rerun column bottom stream temperature has greater effect on the linear alkylbenzene yield than the temperature variation of the top stream. At higher temperature of both streams , lower percentage yield of average wt. % of linear alkylbenzene was obtained with that of the top stream being the lowest at 87.5% as against 93.3% for the bottom stream. The highest linear alkylbenzene yield of 99.4%was recorded at bottom stream temperature of 280oC and pressure of 115Kpa.

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